

## <u>Sebastian Klopotowski<sup>1</sup></u>; Yessica Brachthaeuser<sup>1</sup>; David Mueller<sup>1</sup>; Hendrik Kersten<sup>1</sup>; Walter Wissdorf<sup>1</sup>; Valerie Derpmann<sup>1</sup>; Sonja Klee<sup>1</sup>; Klaus J. Brockmann<sup>1</sup>; Uwe Janoske<sup>2</sup>; Hauke Gregor<sup>2</sup>; Thorsten Benter<sup>1</sup>

### Introduction

The application of atmospheric pressure (API) ionization necessitates a pressure differential pumping stages analysis. One common mass approach for the first reduction step from atmospheric pressure to the low mbar range is realized by critically operated capillaries. The pressure ratio between capillary entrance and first pumping stage is generally greater

than 0.5 leading to choked flow conditions. In fluid dynamical terms the gas flow out of the capillary is a transonic overexpansion. Stationary shock waves (Mach discs), depending on capillary bore and background pressure, are thus expected. The interaction between the gas jet leaving the capillary and downstream ion optical devices (skimmers / ion funnels) could potentially lead to significant ion losses.

The capillary is either actively tempered or heated by a hot dry gas stream.

We used an automated experimental setup to analyze in detail the flow conditions downstream of the transfer capillary exit at various temperatures and pressures.

## Methods

#### **Experimental Methods**

#### Measurement Chamber:

Home built vacuum recipient with mounting for a transfer capillary, evacuated by a flow controlled rotary pump

#### Temperature Probe:

Micro thermocouple (Type K: Ni/CrNi) with 0.25 mm diameter, mounted on a positioning stage behind the capillary exit

#### Capillary:

Home built glass capillary with internal Pt100 measuring resistor, length 18 cm, inner diameter 0.5 mm. Enveloped with tantalum wire (0.1 mm) for current heating

#### XY-Stage:

Moveable platform adjusted by two I<sup>2</sup>C controlled, motorized thread rods

#### **Contact Microfone:**

Directly attached close to capillary exit signals recorded by computer audio interface

### **Pressure Control:**

MKS Type 252E Exhaust Valve Controller between measurement chamber and rough pump with matching butterfly valve.

### Data Acquisition:

Labjack U12 A/D D/A Interface

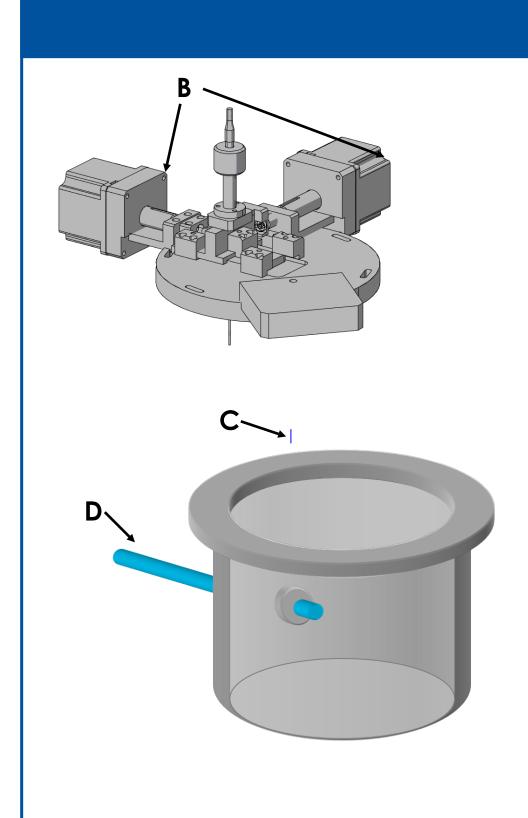
### **Numerical Methods**

### Computational Fluid Dynamics (CFD)

Basic numerical calculations performed with OpenFOAM

#### Fast-Fourier-Transformation (FFT) :

Sound spectrum analysis performed by gnuOCTAVE and plotted with gnuPlot





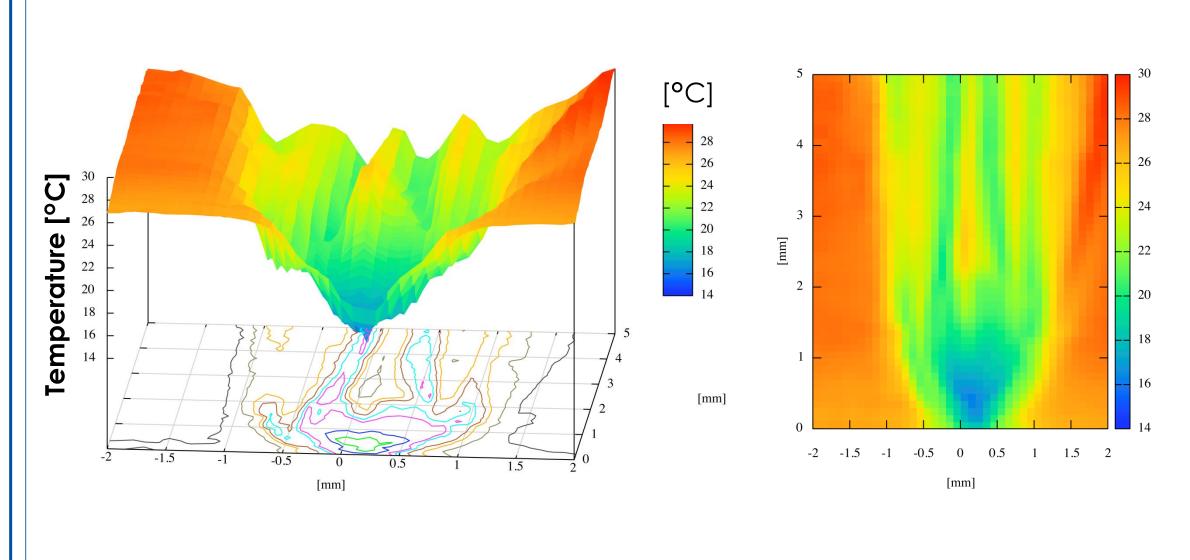
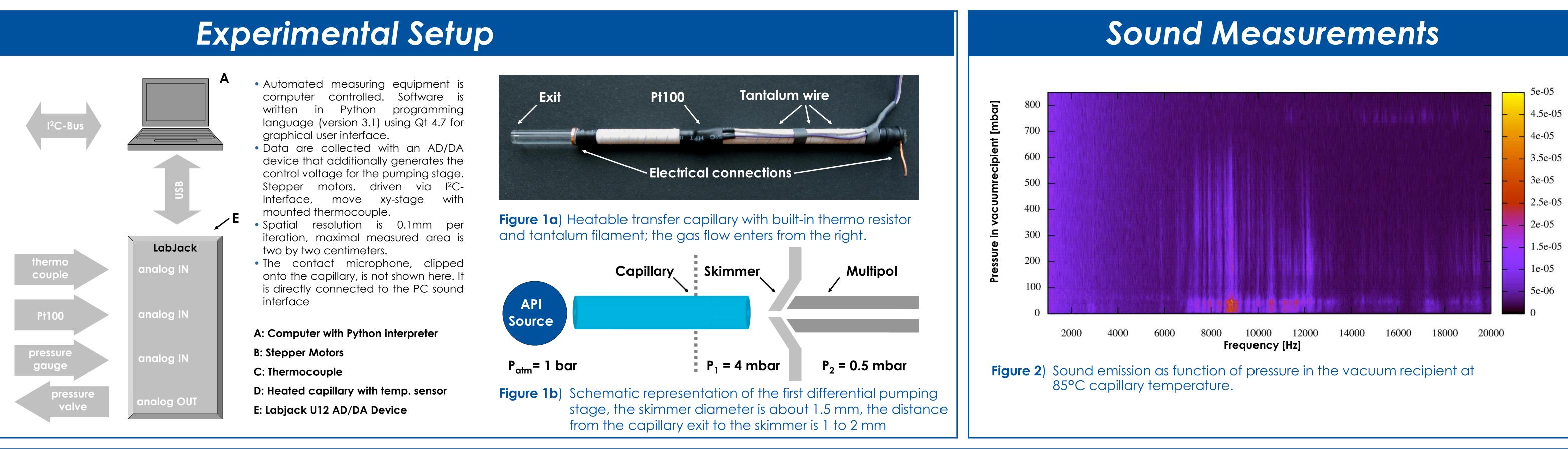


Figure 3a) Results of the temperature measurements in a transonic jet. First shock front is identifiable approximately 2.3 mm behind the capillary exit, width the of gas jet is 2.5 mm

a)  $p_1 = 2 \text{ mbar}$ 23  $\mathcal{M}$ 20 T<sub>cap</sub> = 84°C 0 1 2 3 4 5 **Figure 4)** Temperature distribution along the jet axis for different background

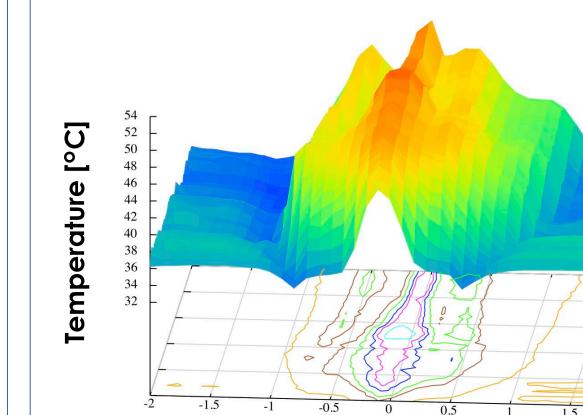
increases.

# **API-MS Transfer Capillary Flow: Examination of the Downstream** Gas Expansion

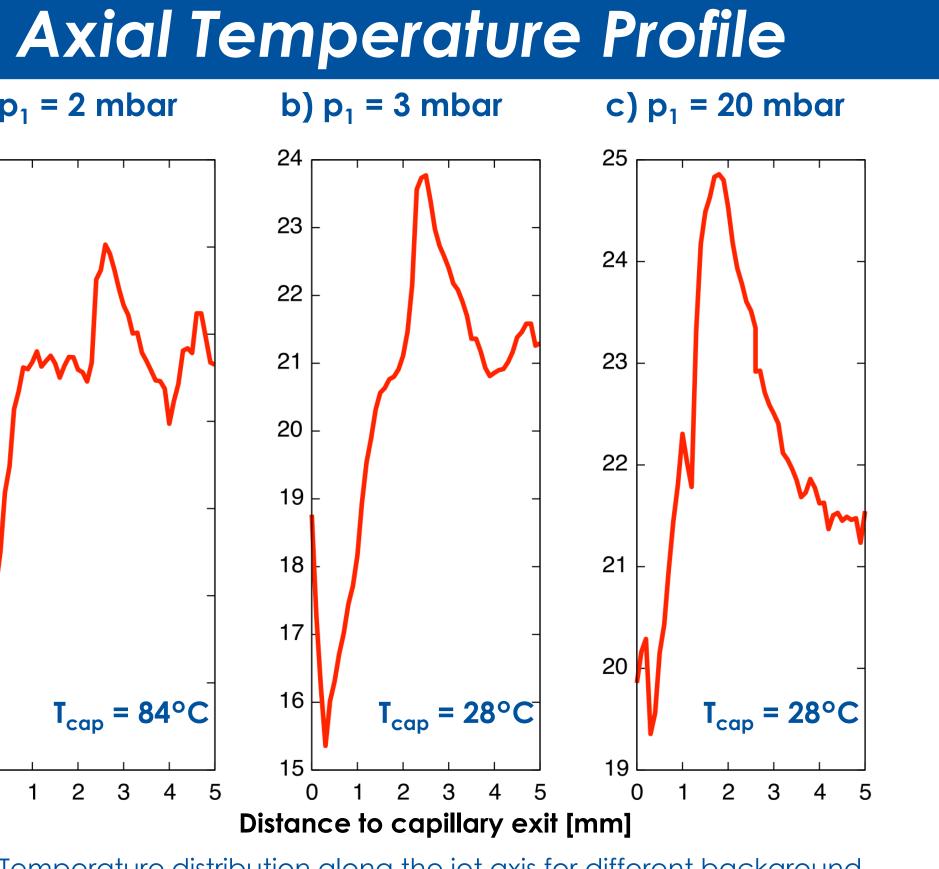




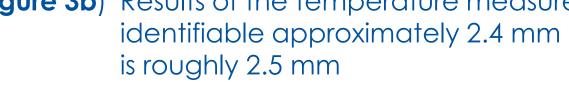
b.) T =  $85^{\circ}C / p_1 = 2 mbar$ 

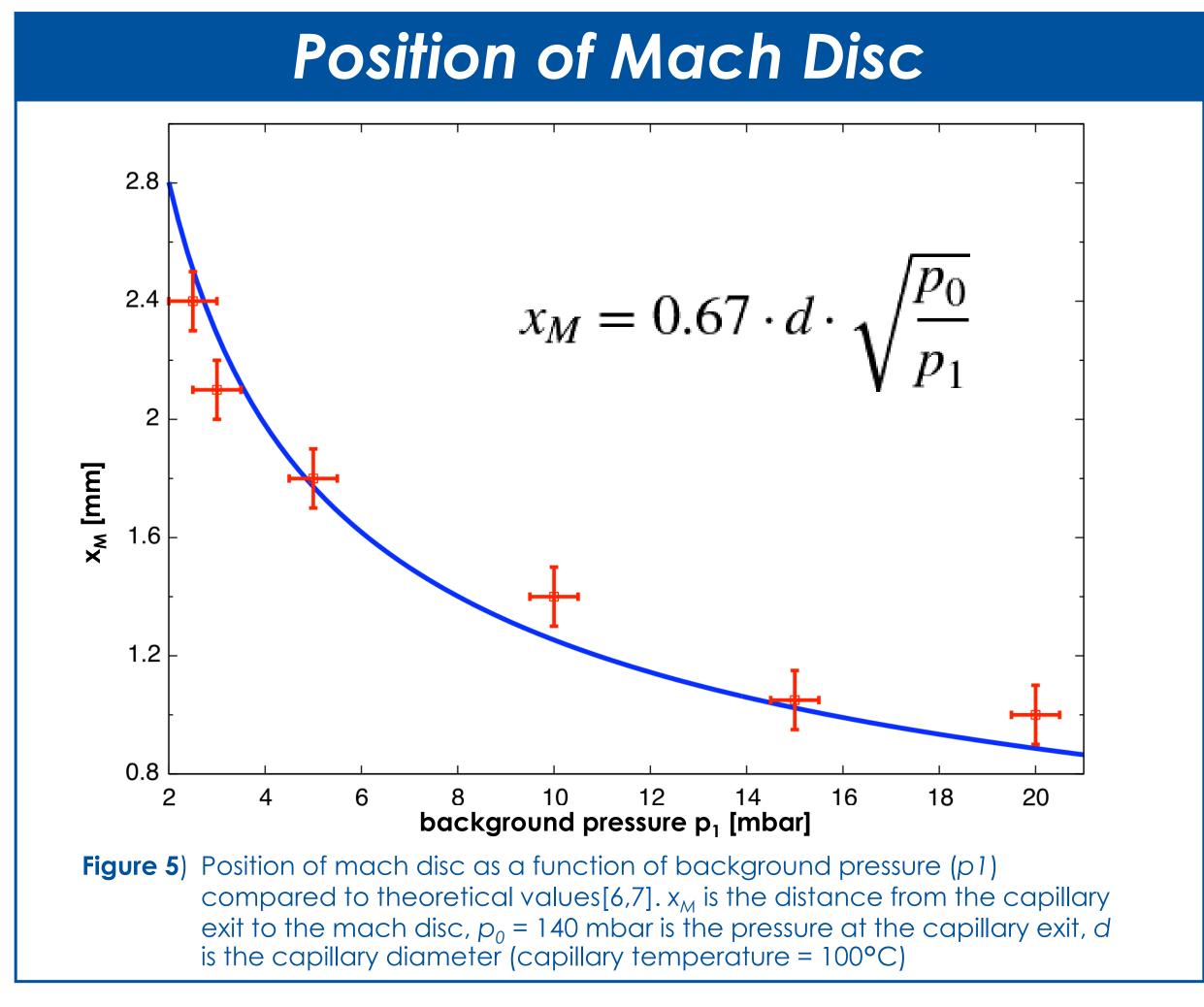


**Figure 3b**) Results of the temperature measurements in a transonic jet. First shock front is identifiable approximately 2.4 mm behind the capillary exit, width of the gas jet is roughly 2.5 mm

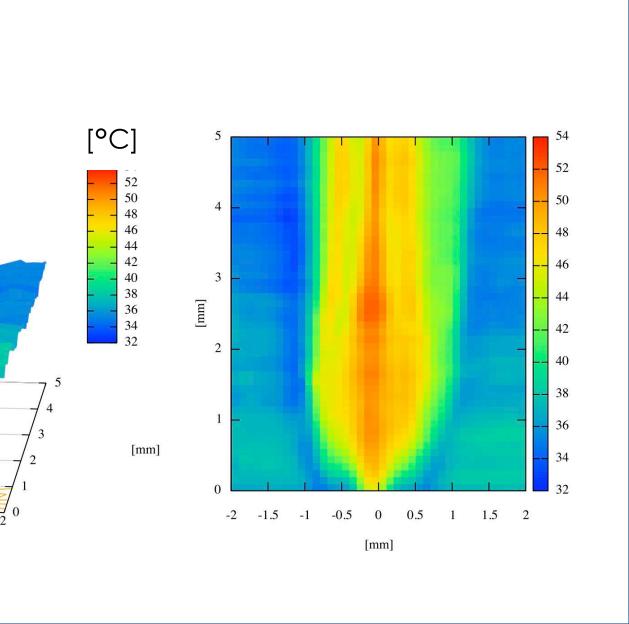


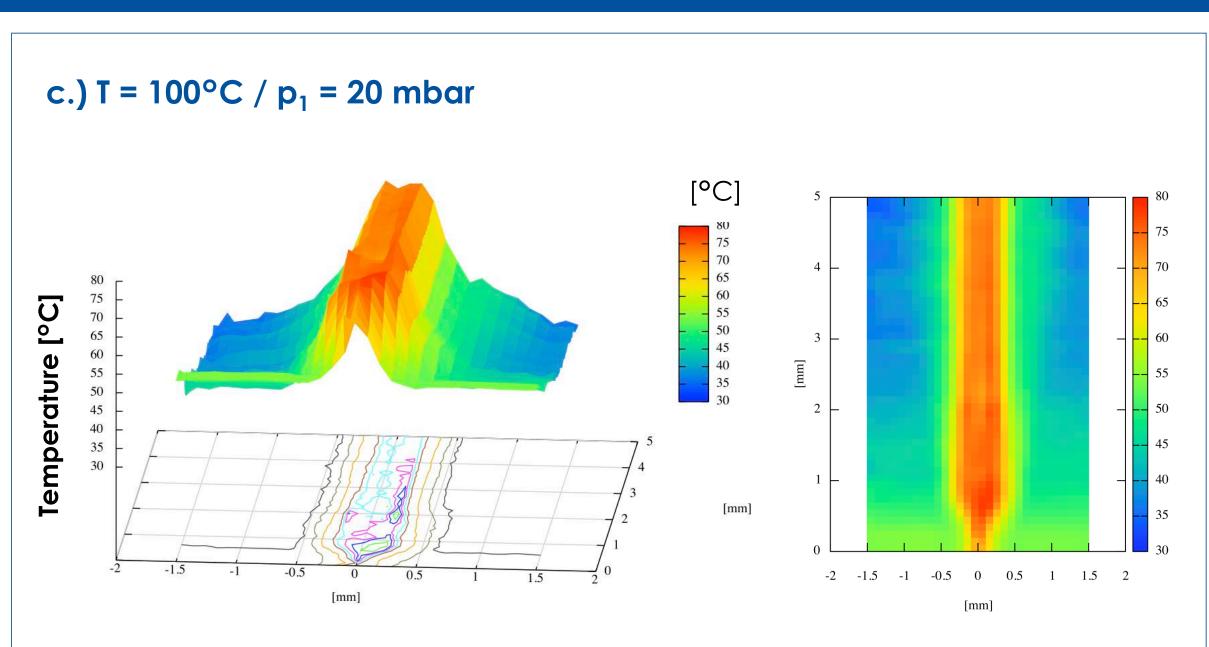
pressures. Shock waves are recognizable by the transient temperature



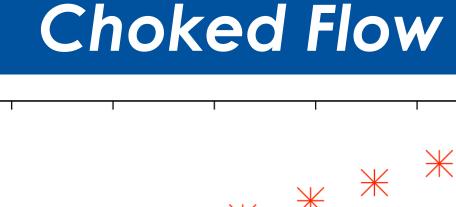


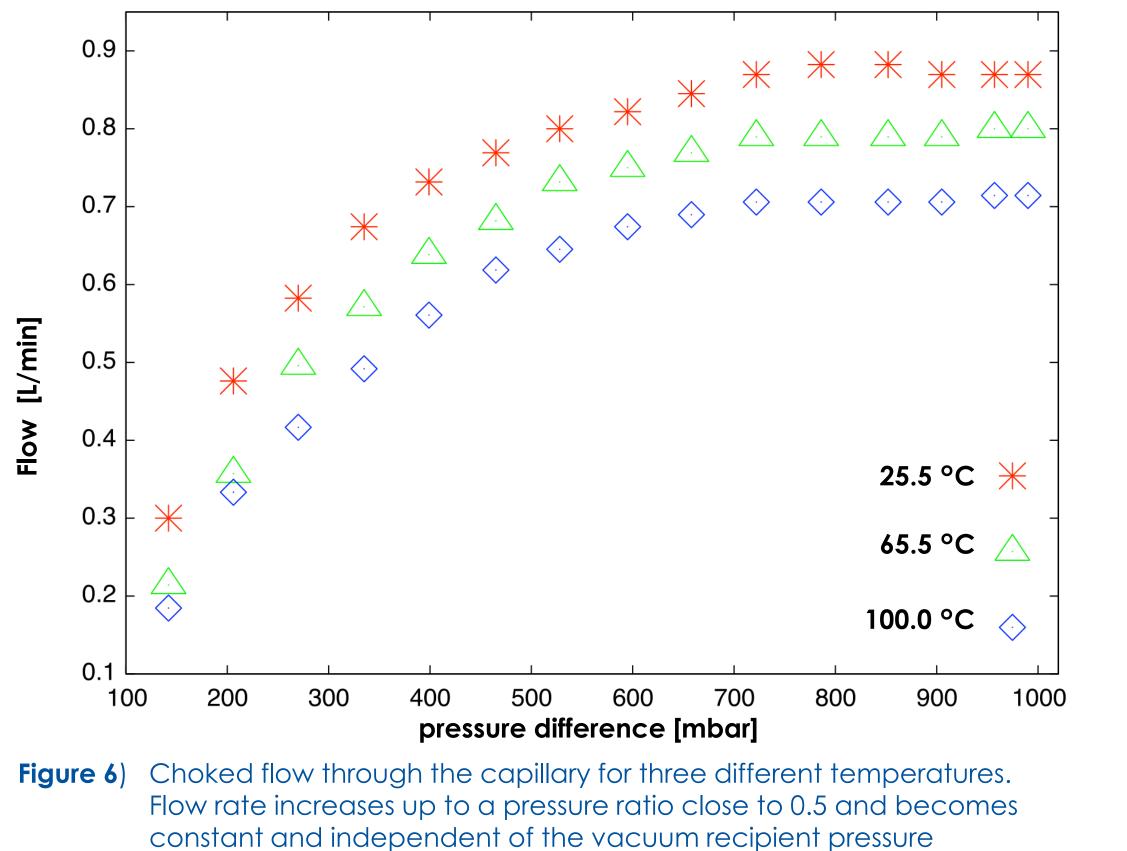
### **Temperature Distribution behind Capillary Exit**





**Figure 3c)** Results of the temperature measurements in a transonic jet. First shock front is identifiable approximately 1.0 mm behind the capillary exit, width of the gas jet is roughly 1 mm







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## Conclusions

- A remarkably narrow and stable gas jet leaves the transfer capillary and can still be measured at some centimeters distance from the exit
- The jet diameter is inversely dependent on the vacuum recipient pressure
- Under typical operating conditions the jet diameter is two to three times wider than the skimmer bore
- Stationary shock waves are observed as sudden increases in the jet temperature, as predicted by numerical calculations
- The Mach disc appears at the expected location irrespective of the capillary wall temperature
- The measured maximum jet core temperature is only marginally lower than the controlled capillary wall temperature
- The minimum temperature in the expansion zone is higher than predicted by the calculations even if the effect of radiation heating by the capillary is considered
- > Interference between jet and skimmer have to be expected
- With rising temperature and viscosity the gas throughput decreases to values that also result from theoretical calculations
- The gas flow is heated effectively even when only the last few cm of the capillary are tempered
- $\succ$  There is not much doubt that the capillary flow is turbulent.
- Transfer capillaries emit characteristic sound spectra, which are dependent on the wall temperature and gas flow
- The frequency spectrum varies with wall temperature but not with recipient pressure
- The highest signal intensities were observed at a recipient pressure of 30 mbar
- Preliminary CFD calculations give an adequate qualitative picture of the overexpanded flow; additional investigations are underway

### Literature

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