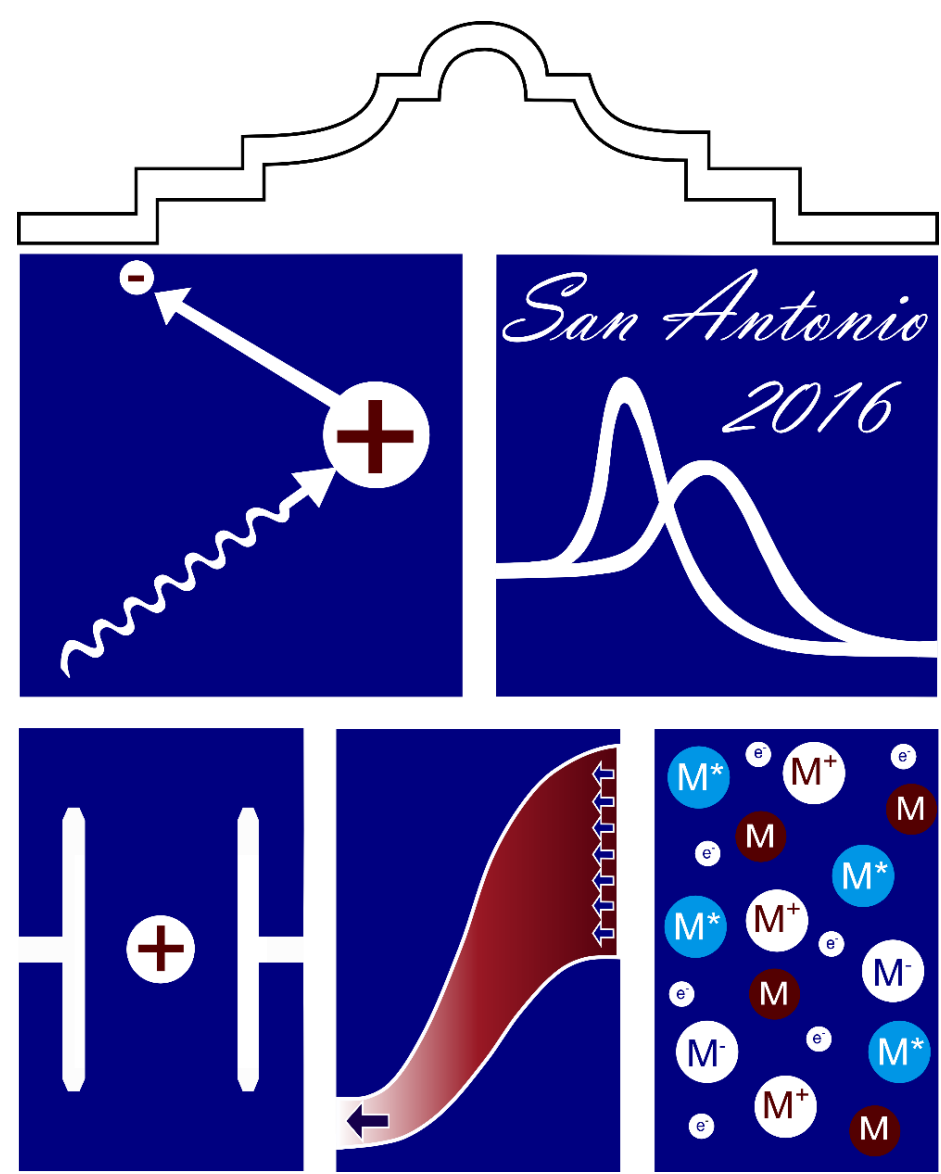




# Development and Optimization of an inlet system for Desorption Atmospheric Pressure Photoionization – Mass Spectrometry (DAPPI-MS)



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## Introduction

At the 56<sup>th</sup> Annual ASMS Conference on Mass Spectrometry and Allied Topics the Vapur® API Interface was presented [1] and patented in 2010 by Ionsense Inc. (Saugus MA, USA) [2].

The Interface was designed to improve the collection efficiency of desorbed ions generated by ambient pressure desorption ionization sources, such as DART [3]. A factor of 500 increase in sensitivity for the analysis of Verapamil directly from rat plasma and a significant improvement in the overall sample-to-sample reproducibility was reported. The patent holders deem the “jet separator effect” as the physical principle behind the observed progress in sensitivity [2].

This effect allows to efficiently separate the heavier analyte molecules from the lighter carrier gas due to fluid dynamic properties within a jet expansion.

In this contribution a comparable interface was optimized for the application in desorption atmospheric pressure photoionization (DAPPI) [4]. Along the work the proposed working principle was carefully scrutinized.

## Methods

**MS** Xevo Qtof, Waters Corporation, Milford, MA, USA

**Ion Source** APPI with a Microchip Heated Nebulizer (micro-APPI) [5]  
100 ml/min nitrogen  
3  $\mu\text{L} \cdot \text{min}^{-1}$  liquid sampling flow

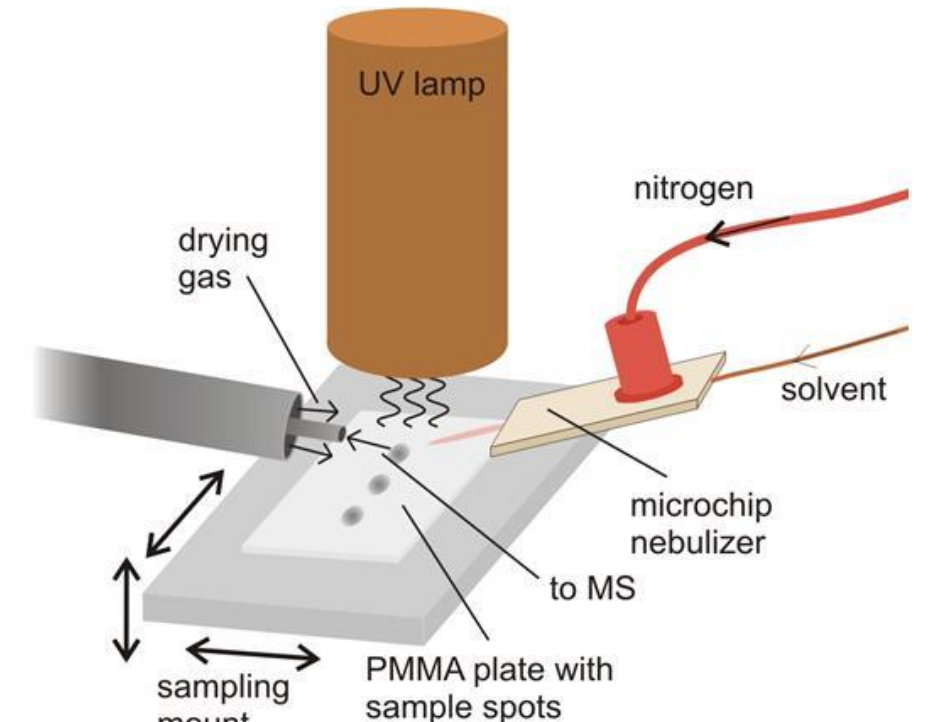
**Radiation Source** VUV Kr discharge lamp (Heraeus Noblelight GmbH, Hanau, Germany)

**Analytes** Mix 1:  
testosterone (1  $\mu\text{M}$ ), benzo[a]pyrene (1  $\mu\text{M}$ ), 1-naphthol (2  $\mu\text{M}$ ), cholesterol (2  $\mu\text{M}$ ), creatinine (2  $\mu\text{M}$ ), verapamil (2  $\mu\text{M}$ ), C12-ceramide (10  $\mu\text{M}$ )

Mix 2:  
testosterone (10  $\mu\text{M}$ ), benzo[a]pyrene (10  $\mu\text{M}$ ), 1-naphthol (10  $\mu\text{M}$ ), cholesterol (10  $\mu\text{M}$ ), creatinine (10  $\mu\text{M}$ ), verapamil (10  $\mu\text{M}$ ), C12-ceramide (10  $\mu\text{M}$ )

**Vacuum pump** Rotary Vane Vacuum Pump TRIVAC type D16B (Leybold Vakuum GmbH, Bonn, Germany)  
Capacity: 16  $\text{m}^3 \cdot \text{h}^{-1}$

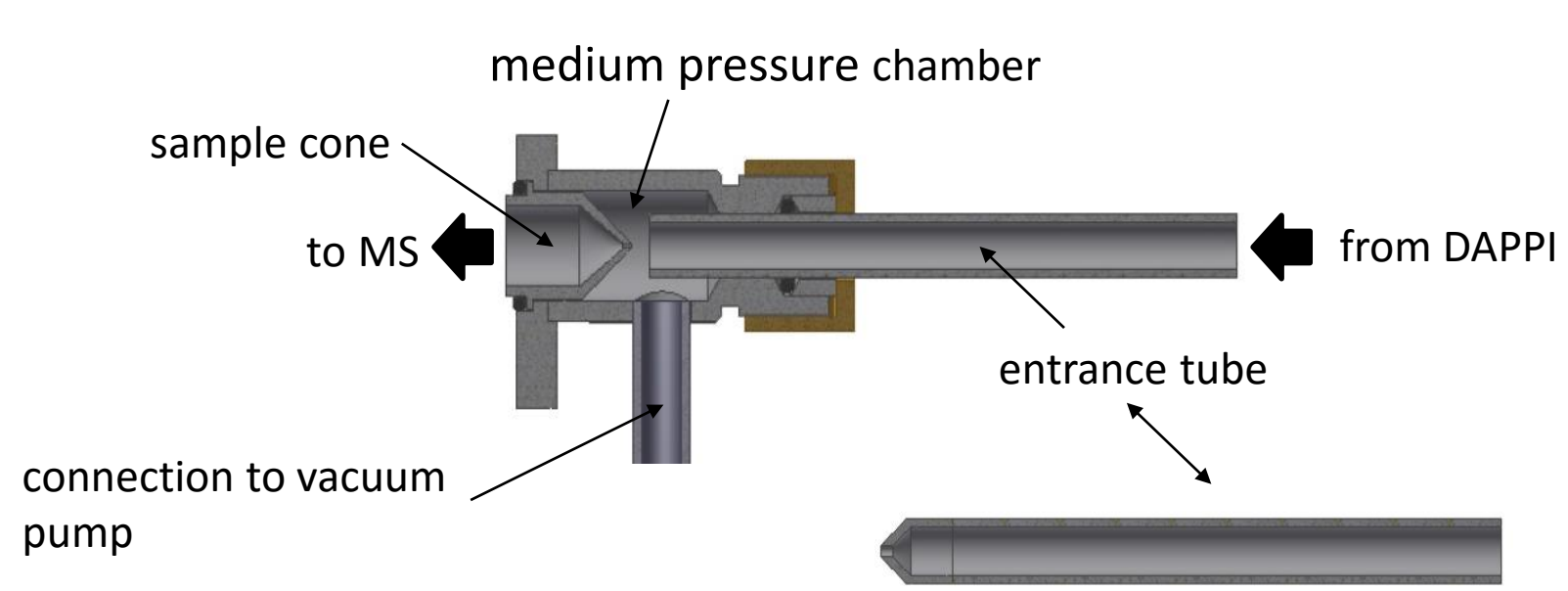
## Method - DAPPI



**Figure 1:** A schematic of the desorption atmospheric pressure photoionization (DAPPI) setup.

- A heated nebulizer microchip sprays a hot plume consisting of nitrogen gas and vaporized solvent
- The hot vapor jet is directed towards the sampling surface  
→ Thermal desorption of analytes to gas phase
- A krypton discharge lamp emits 10 eV photons that ionize the solvent  
→ gas-phase reactions lead to ionization of the analytes

## Inlet System Design



**Figure 2:** A schematic of the developed DAPPI inlet system

The developed inlet system is designed along the line of the Vapur API interface for Direct Analysis in Real Time (DART) [3]. A vacuum pump connected to the medium pressure chamber maintains an increased, regulated volume flow through an entrance tube. Different entrance tubes (cf. Table 1), for example with a convergent nozzle at the low pressure end

of the tube nozzle allowed a directed gas flow onto the MS inlet sample cone. Due to its reduced inner diameter (i.d.) this nozzle enables a choked flow. The gap distance between the entrance tube and the MS inlet sample cone can be varied. For a better ion focusing a potential gradient can be applied between the entrance tube and the sample cone. Additionally the entire interface can be heated.

| no. | sample cone    |                                            | no. | entrance tubes |                                            | no. | entrance tubes with nozzle |                  |                                            |
|-----|----------------|--------------------------------------------|-----|----------------|--------------------------------------------|-----|----------------------------|------------------|--------------------------------------------|
|     | cone i.d. [mm] | choked volume flow* [L·min <sup>-1</sup> ] |     | tube i.d. [mm] | choked volume flow* [L·min <sup>-1</sup> ] |     | tube i.d. [mm]             | nozzle i.d. [mm] | choked volume flow* [L·min <sup>-1</sup> ] |
| 1   | 0.36**         | 1.2                                        | 1   | 1              | 7.9                                        | 4   | 2                          | 1                | 9.4                                        |
| 2   | 0.5            | 2.4                                        | 2   | 2              | 26.2                                       | 5   | 2                          | 1.5              | 21.2                                       |
| 3   | 1.0            | 9.4                                        | 3   | 5.1            | -                                          | 6   | 5.1                        | 1                | 9.4                                        |
|     |                |                                            |     |                |                                            | 7   | 5.1                        | 1.5              | 21.2                                       |

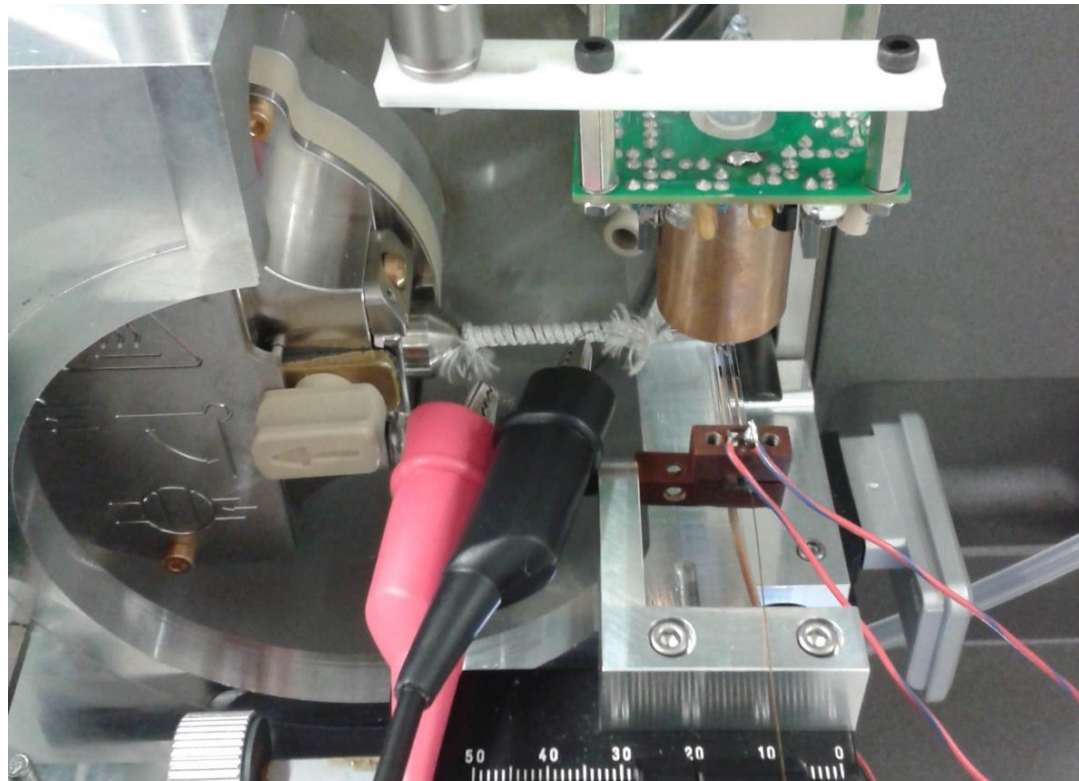
**Table 1:** Overview of the different entrance tube and MS inlet sample cone geometries.

\* Calculated from Ref. [6]; \*\* original MS inlet sample cone

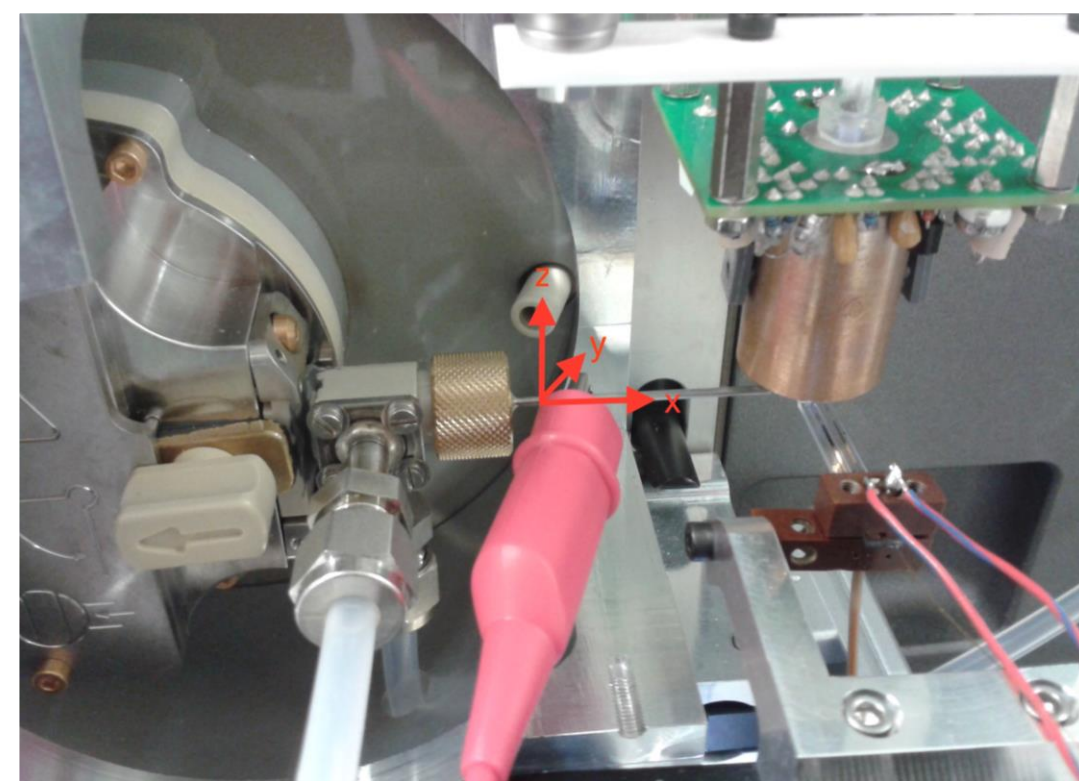
## Experimental Setup

To reduce the set of parameter and to provide a continuous and stable sample introduction, the new interface was characterized and optimized using micro-APPI [5]. For the iterative optimization of the ion transmission, several parameters (listed in section: Inlet System Design) were carefully assessed.

The sample solution was infused with a syringe pump (3  $\mu\text{L} \cdot \text{min}^{-1}$ ) and nitrogen was used as the microchip nebulizer gas (100  $\text{mL} \cdot \text{min}^{-1}$ ). The microchip was mounted on a xyz-stage, which enabled an exact and reproducible spatial alignment of the assembly. The microchip was further resistively heated with a common DC power supply. Performance improvement of each source development iteration step of the new inlet system was carefully assessed with comparative measurements of a sample mixture containing pharmaceutically relevant substances. Depending on the flow restrictions of the entrance tube and sample cone (cf. Table 1) the connected vacuum pump allowed to maintain background pressures in the interface enclosure ranging from 100 mbar to 1000 mbar. The pumping speed was regulated with a swagelok valve and the pressure is monitored with a commercial barometer.



**Figure 3:** The conventional micro-APPI setup



**Figure 4:** The developed inlet system setup for micro-APPI

## Theory and Questions

Due to vacuum restrictions, most LC/MS instruments collect only a small fraction of the desorbing gas (cf. Figure 5, left). Typical volume flows of these instruments range between 1 and 2  $\text{L} \cdot \text{min}^{-1}$ . Enhancement of the ion collection efficiency from the desorption/ionization region can be achieved by increasing the volume flow of the gas transporting the desorbed analytes.

With an additional differentially pumped stage more of the desorbing gas plume containing analyte ions is collected (cf. Figure 5, right)

If the pressure ratio becomes sufficiently high, a free jet under continuum conditions would form (cf. Figure 6). In this case, compounds with high diffusivity would be deflected from the central flow axis (jet separation effect). The diffusivity is proportional to the root of the inverse mass. Thus the lighter background gas would diffuse more than the heavier analyte ions. Consequently, a reduction of the volume flow and an enrichment of the analyte would be achieved.

**Boundary Conditions** for a free jet expansion under continuum conditions.

For continuum flow characteristics the gas has to be sufficiently dense, as expressed with the Knudsen number  $K_n$ :

$$K_n < 0.01 \quad K_n = \frac{\bar{l}}{d}$$

$\bar{l}$  = Mean free path  
 $d$  = diameter flow channel

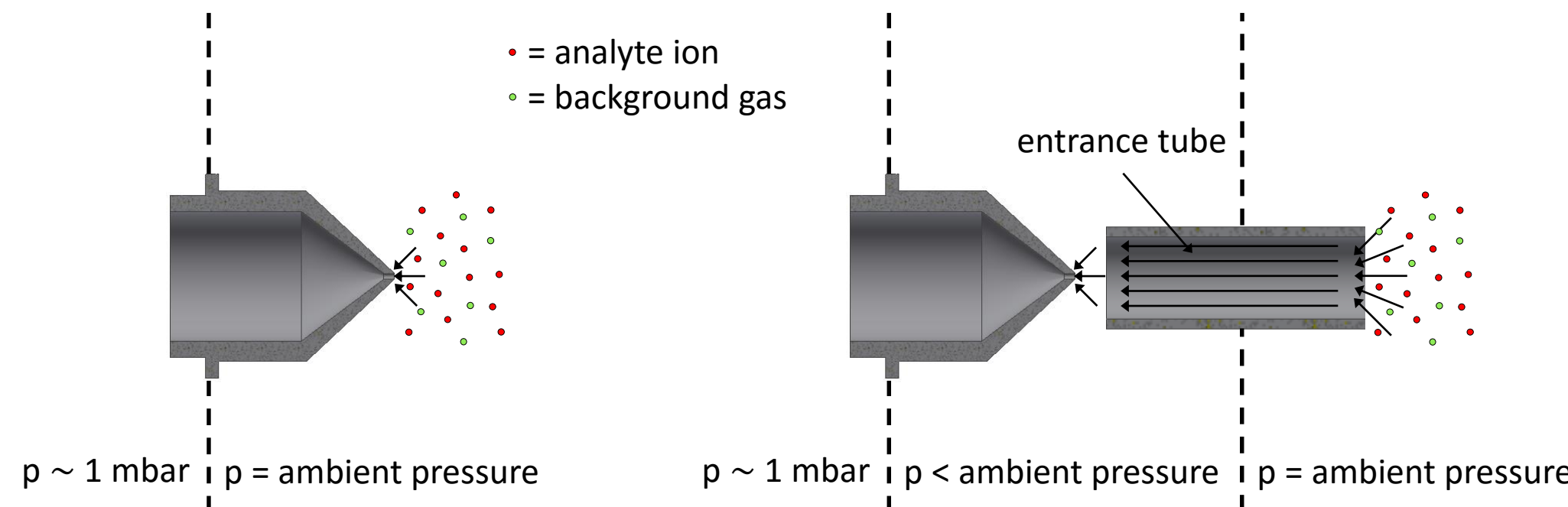
To form a jet, the pressure ratio  $\frac{P_0}{P_1}$  has to be  $> 15$  [7]. In this case the position of the mach disk is calculated by:

$$x_m = 0.67 * D_0 * \sqrt{\frac{P_0}{P_1}}$$

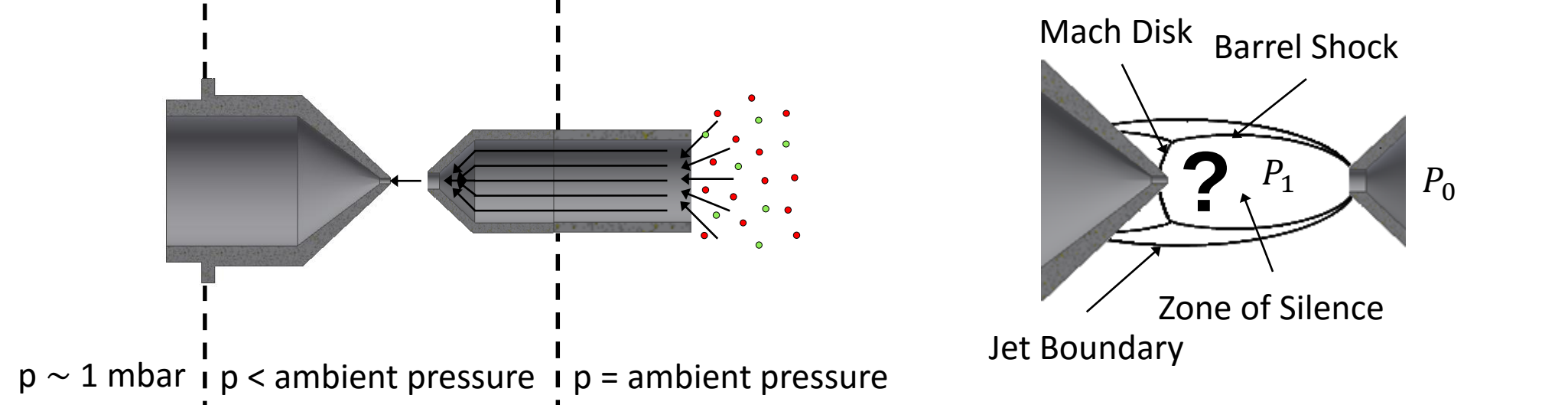
$x_m$  = location of mach disk  
 $D_0$  = nozzle diameter

$P_0$  = upstream pressure  
 $P_1$  = downstream pressure

For the original Vapur API Interface configuration the estimated total maximum pressure drop is 10 mbar. Accordingly, the pressure ratio is near unity, which renders the jet formation under these conditions unlikely. The observed intensity and stability increase is most probably attributable to a simple improved collection efficiency of the desorbed material.



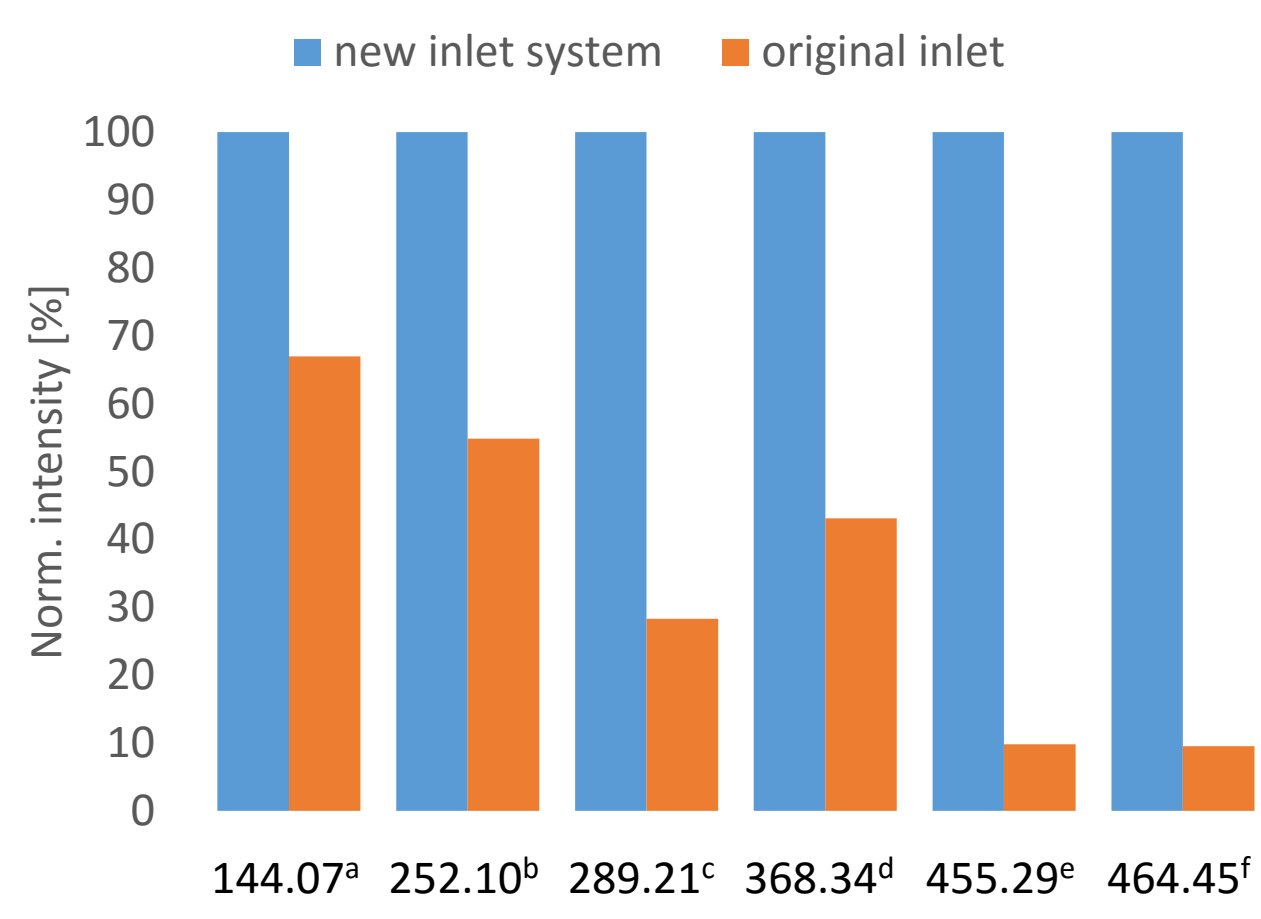
**Figure 5:** Left: A schematic of the conventional MS inlet sample cone. Right: A schematic of the Vapur API interface.



**Figure 6:** Left: A schematic of the new inlet assembly with a convergent nozzle at the low pressure region. Right: Enlarged section of the gap region and the proposed jet expansion.

## Results

**Figure 7:** Comparison between the new inlet system and original inlet. Summed ion signals (1.5 min) of selected analyte masses: <sup>1</sup>naphthol (MH<sup>+</sup>), <sup>2</sup>benzo[a]pyrene (M<sup>+</sup>), <sup>3</sup>testosterone (MH<sup>+</sup>), <sup>4</sup>cholesterol ([M-H<sub>2</sub>O]<sup>+</sup>), <sup>5</sup>verapamil (MH<sup>+</sup>), <sup>6</sup>C12-ceramide ([MH-H<sub>2</sub>O]<sup>+</sup>)



Mass spectra with the new inlet system show lower background. Furthermore, a comparison of the mass range from  $m/z = 50$  to  $m/z = 250$  indicates discrimination of lower masses with the new inlet system. This trend is also seen in Figure 7. The relative intensity gain increases with higher  $m/z$ . The reason for these observations is still under investigation.

